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AN9006

IGBT Application Note For Camera Strobe

Camera Strobe System Summary

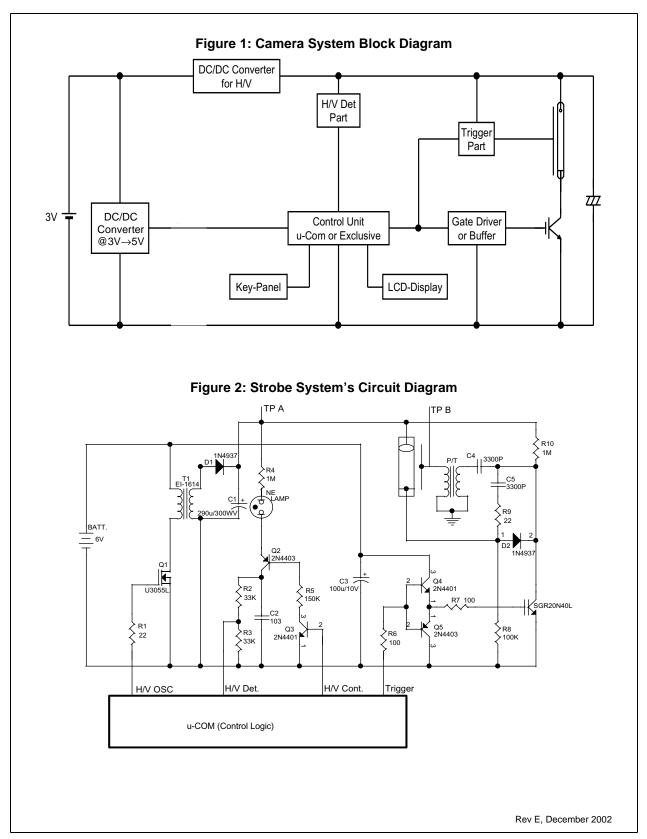
The Camera Strobe System (Portable & DSC) is a lighting system for taking pictures in relatively dark areas, without the accompanying negative effect on picture quality. The strobe system is becoming smaller, lighter and easier to control, increasing the popularity of DSC and portable automatic cameras.

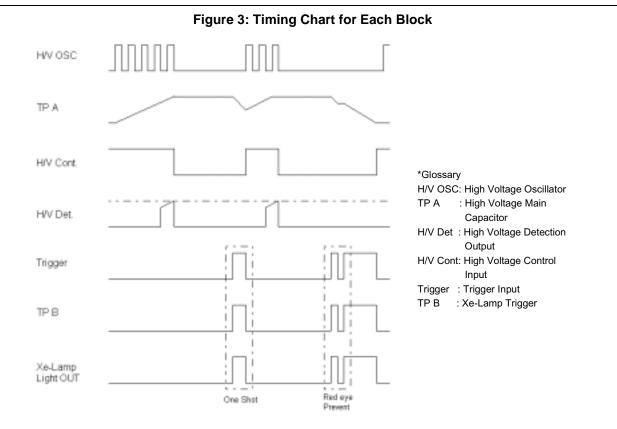
1) Strobe System Control Methods

The control methods are largely divided into two groups: One uses SCR, and the other uses IGBT. The advantages and disadvantages of both methods are compared below:

ltem	SCR Control	IGBT Control	Remarks
Circuit Configuration	Complicated	Simple (Can be directly operated from Logic)	
Current Capacity	Up to hundreds Amp.	Up to 150A (@ logic level)	
Disadvantages	 Low battery efficiency (full electric discharge) Hard to achieve red eye prevention function Need SCR for turn-off Limitation in luminosity control 	High intensity luminosity is difficult.	
Advantages	High intensity luminosity is possible	 Fast response time Red eye prevention function is possible High battery Efficiency 	

Table 1: Comparison of Control Methods





< Timing Chart for Each Block>

2) Control Power Block Configuration

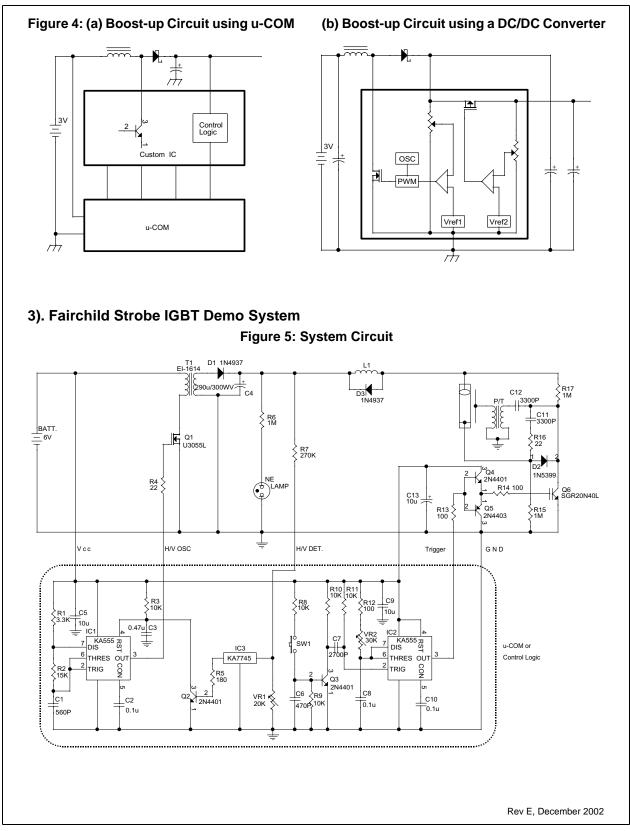
Portable cameras and DSC use 3 V or 6 V batteries, but lately the 3 V battery is becoming more prevalent. When using a 3 V power source, the IGBT's gate drive Voltage is insufficient, even with a logic level IGBT. Hence, a boost-up circuit is reequired for DC power voltage. The boost-up circuit, used in a portable strobe system, is divided into two types.

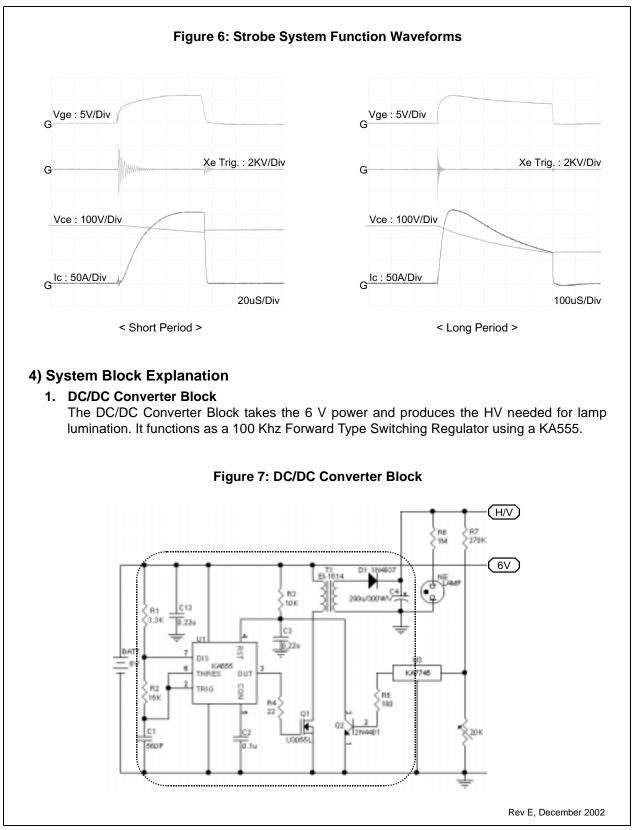
1. Boost-up circuit using u-COM

The circuit has the PWM Controller function built-in within the u-COM for system control, and produces about 100-150 Khz of S/W frequency for reducing transformer size. Duty control functionality is also available.

2. Boost-up circuit using a DC/DC Converter

This is the most commonly used circuit. It is used independently without the control of a u-COM. The converter used, most often, is the RS5RM series type with RICOH's PWM and built in voltage detection. This circuit mainly boosts 3 V power up to 5 V. It has a switching frequency of 50 Khz, and the duty is variable up to a maximum of 90%. When the output voltage is lower than a specific value, it is compensated for by increasing the duty. When it is higher than a set value, it saves energy in the coil while the internal TR is on. When the TR is turned off, the 3 V power voltage and organic voltage are combined to provide 5 V output.





The switching frequency and duty are set by the resistance (R1) between KA555`s V_{CC} and Pin 7, the resistance (R2) at connecting pins 7, 6 and 2, and the capacitor (C1) value. f = 100 Khz (@ T = 10 μ S) Ton = 4.5 μ S, Toff = 5.5 μ S Toff = 0.67 * R2 * C1 (Here, C1 = 560 pF) Rb = Toff / (0.67 * C1) = 5.5 μ S / (0.67 * 560 pF) = 14658 Ω (here the standard resistance is 15 k Ω) Ton = 0.67 * (R1+R2) * C1 Duty = R2 / (R1+R2) = 0.45 = 15k Ω / (R1+ (2 * 15 k Ω) R1 = 3.3 k Ω

KA555's pin 4 (Reset) receives a signal detected in Block 2's HV, and is able to stop KA555. The Reset block (4) changes to Reset mode between 0.4 and 1.0 V (Min/Max), so you must be careful with the voltage level.

2. Design of the Boosting Transformer

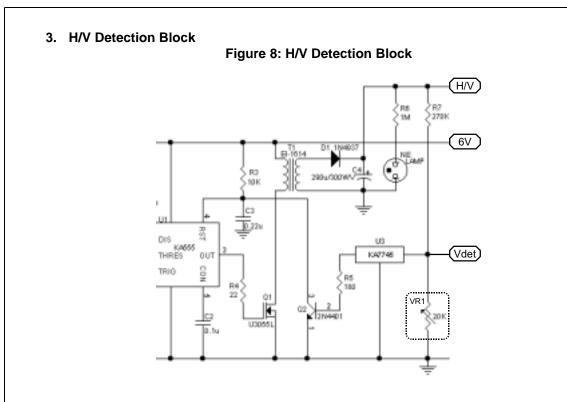
The transformer's size is EI-1614. A smaller size is better for making the product smaller and lighter. In this design the most commonly available smallest size is used.



First calculate the 1st order coil Np. Then calculate the 2nd order coil Ns. Np = (Vin * ton / B * Ae) * 108 = (6V * 4.5uS / 2200G * 0.1982) * 108= 6.19 T (approximately 6T)

(The battery's voltage failure and a discharge of up to 5.2 V are factored into the design) Ns = (Vs * Np) / Vin(min)

= (300V * 6T) / 5.2V = 346.15T (approximately 346T)



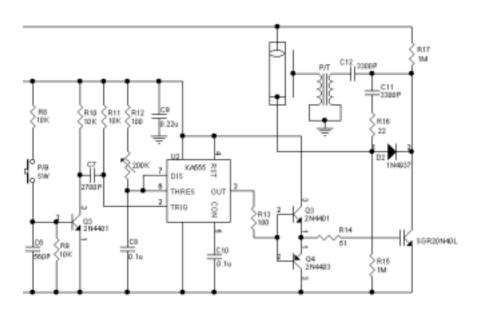
This block detects voltages from 250 to 300 V and controls Block 1. It uses the component KA7745 for voltage detection(detection volt: 4.5 V).

When Vdet. block's voltage is below 4.5 V, the KA7745's output is low, and when it is over 4.5 the output is high. The high output activates Q2, lowers KA555's pin 4's level, and stops the DC/DC converter by putting it in a Reset Condition. The voltage is detected by dividing HV using resistance, and HV is set to the required value (200-300 V) using VR1. The NE-lamp shows the condition of the energy stored in the capacitor.

4. Strobe Light Duration Control Block for Lighting Duration

This block outputs a trigger signal using the Time IC KA555, activating it to mono-stable mode, and by receiving an external trigger signal. The output pulse (duration of luminescence) is adjusted using the Rt and Ct connected to pins 6 and 7 on the KA555.





In mono-stable mode, T = 1.1 * Rt * Ct. Hence, the Xenon-lamp's luminescence duration is maintained between the following:

 $T(min) = 1.1 * 100\Omega * 0.1\mu F = 11\mu s$

 $T(max) = 1.1 * 200.1 k\Omega * 0.1 \mu F = 22 ms$

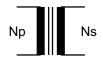
The KA555 has a source/sink capability of upto 200 mA, and directly activates the IGBT (SGR20N40L). But in this system a Buffer Block is added using TR just in case there is a shortage of gate drive capability.

- SGR15N40L and SGR20N40L are logic level IGBTs, and can be operated directly from many different types of logic ICs, as long as the control logic part's output current is above 100 mA.

5. Strobe Unit

This unit is composed of the Xenon lamp and the trigger transformer. The trigger pulse ionizes the gas mixture within the Xenon lamp. It also receives a signal (about 250-300 V) when the S/W element IGBT is on, and produces an HV trigger signal of about 4 to 5 kV by using the pulse transformer's turn number and ratio. The pulse transformer can be designed as follows.

$$V(trig) = \frac{N2}{N1} \times Vin$$



The Vin is about 250 to 300 V, and the voltage is determined by the turn ratio. If the trigger pulse voltage is low, the Xenon lamp does not luminate or does so irregularly. If it is too high, the Xenon lamp's electrode may discharge or damage other parts nearby. The trigger pulse output wire should be as close as possible to the Xenon lamp trigger's electrode.

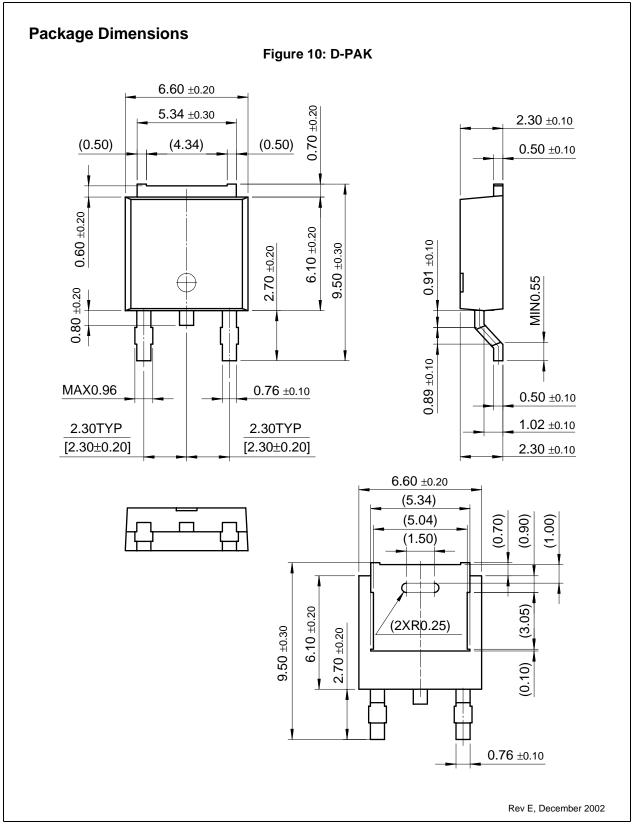
5). Notes for Constructing a Strobe System

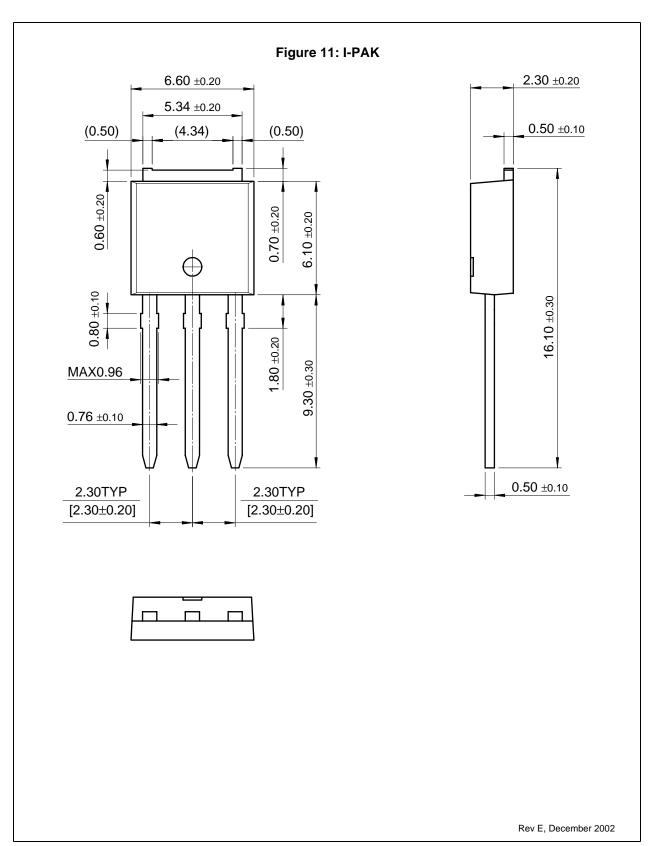
- The energy capacity of a small strobe lamp is below 20 W-S, and it should not be exceeded. (refer to the of the Xenon tube specifications)
- The P/T (trigger transformer) should be designed for an output of about 4 to 5 kV. If it is too low, the Xenon lamp does not luminate or does so irregularly. If it is too high, the Xenon lamp's electrode discharges and may damage neighboring parts.
- The wire between the energy storing capacitor and the Xenon lamp should be as short and thick as possible.

Gate Drive	Rating					
Volt. [V]	V	Α	FAIRCHILD	Mitsubishi	Toshiba	Remark
4.5	400	130	SGR15N40L	CT20ASJ-8	GT5G103	D-PAK
			SGU15N40L			I-PAK
		150	SGR20N40L	CT25ASJ-8	GT8G103	D-PAK
			SGU20N40L		GT8G121	I-PAK

Table 2: FAIRCHILD Strobe IGBT Line-up & Competitor

Comparison of Fairchild Strobe IGBTs with Competitors'





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CoolFET™	FASTr™	MicroFET™	PowerTrench [®]	SuperSOT™-6
CROSSVOLT™	FRFET™	MicroPak™	QFET™	SuperSOT™-8
DOME™	GlobalOptoisolator™	MICROWIRE™	QS™	SyncFET™
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E ² CMOS™	HiSeC™	MSXPro™	Quiet Series™	TruTranslation™
EnSigna™	I ² C™	OCX™	RapidConfigure™	UHC™
Across the board.	Around the world. [™]	OCXPro™	RapidConnect™	UltraFET [®]
The Power Franch	nise™	OPTOLOGIC [®]	SILENT SWITCHER [®]	VCX™
Programmable Ac	tive Droop™	OPTOPLANAR™	SMART START™	

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