

AN-0000 SPM 2 Package Assembly Guidance

For 32L (FSAM-) and 34L (FNA-)

1. Introduction

Fairchild SPM 2 series is a compact semiconductor power module in Dual Inline with high-functionality and high efficiency. Target applications are motor drives for industrial use such as air conditioners, general-purpose inverters, and servo motors. Proper mounting is required to achieve good thermal performance and low mechanical stress during lifetime of the device. Figure 1 shows the assembly process flow for SPM 2 32L and 34L packages. Assemblies commonly are done using method 1 or method 2 by customer's determination. This application note is intended to provide recommendations for proper handling, assembly of the package and potential rework in conjunction with industry standards. Following sections outline appropriate TIM (Thermal Interface Material) application and heat sink mounting as well as soldering procedures to ensure a reliable PCB (Printed Circuit Board) connection. Recommendations in this note are based on simulation and experimental results from laboratory and field tests.



Figure 1. SPM 2 Module assembly process flow

2. General Package Information

2.1. Package surface specification

The measurement area for the flatness of the package surface is specified by the package center and the four outside corners, as shown in Figure 2. Flatness for the SPM 2 is specified in Table 1. The surface shows a convex bow shape but when the module is screwed down with torque, the thermal compound spreads out and fills the air gaps between the two contact partners, finally ensuring full contact.

SPM2 32L





	Min.	Тур.	Max.
SPM2 32 L	0		+120 um
SPM2 34 L	0		+200 um

2.2. Heat sink surface specification

An heat sink is a passive heat exchanger that is designed to absorb and disperse heat away from the power devices. The thermal performance of a module is influenced by the quality of the surface contact to the heat sink. To optimize the thermal dissipation it is required to maintain a high quality of the heat sink surface. Surface flatness and roughness are the key factors to be considered when manufacturing the heat sink. In order to obtain the maximum thermal conductivity of heat sink and module, the specification given in Table 2 and Figure 3 needs to be followed. The surface of the heat sink must be clean and free of particles. Besides the surface quality, the heat sink design is also one of the key factors that improve the heat dissipation capability of a device.

Table 2.	Heat sink surface	requirements
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(a) Flatness of heat sink	-50 ~ 100 (µm)
(b) Geometrical surface	$\leq\!10$ (µm) to DIN EN ISO
roughness (Rz)	4287



2.3. Specification of external terminals

Table 3 shows technical features of the external terminals. The capability of the leads in terms of pulling and bending are evaluated to check the devices to withstand stresses from actual handling and assembly of the devices in application. The heat resistance of the terminal is also evaluated according to JESD22-B106.

Table 3.Mechanical characteristics of externalterminals

Parameter		Description
Main material		Cu Alloy
Material	Plating material	Ag partial plating
	Thating matchai	(min. 3 um)
Pulling strength, Load 19.6 N acc. to EIAJ-ED-4701		Min. 10 sec
Bending strength, Load 9.8 N 90 deg. bend acc. to JESD22-B105-C		Min 2 times
Heat resistance test acc. to JESD22-B 106		260±5°C, 10±1 s

2.4. Clearance and creepage distance

Since electrical isolation is directly related to the reliability of the product and its safety, it is considered as an important design factor of a power package. The spacing distance between components that are required to withstand a given working voltage and the environment (depending on the pollution degree, temperature and relative humidity) is specified in the terms of Clearance and Creepage in IEC 61800-5-1. Clearance is defined as the shortest distance through the air between two conductive parts. Creepage is defined as the shortest path between two conductive parts measured along the surface of an isolator.

The specification of the electric spacing between the leads is described in Table 4 and 5 as well as in Figure 10 and 11. After heat sink mounting, the minimum clearance and creepage distance between the leads and the heat sink are 3.8 mm and 6.06 mm respectively. In order to maintaining certain spacing addressed in the relevant standard after heat sink and PCB assembly, creepage and clearance need to be checked and additional measures to enlarge the creepage

and clearance distances may need to be applied. Figure 6 shows one of example how to achieve the enlarger creepage and clearance by modify the heat sink shape.

 Table 4.
 Minimum distance for isolation for 32L

Location	Clearance [mm]	Creepage Distance [mm]
A. Between Power Terminals	4.42	4.62
B. Between Control Terminals	2.70	4.90
C. Between Terminals & H/S	3.00	4.30

Table 5. Minimum distance for isolation for 34L

	Location	Clearance [mm]	Creepage Distance [mm]
D. Be	tween Power Terminals	7.80	8.00
E. Between Control Terminals		3.05	6.85
F. Between Terminals & H/S		3.80	6.06



Figure 4. Distance for isolation from Pin to Pin and from Pins to Heat Sink (SPM2 34L)



Figure 5. Distance for isolation from Pin to Pin and from Pins to Heat Sink (SPM2 32L)



Figure 6. Creepage and Clearance improvements by heat sink modification

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3. Assembly Sequences

The assembly process can be done in two ways. One method is mounting the module onto the heat sink first and then proceed with soldering. (Section 3.1) On the contrary, soldering the module on the PCB can be done first, then mounting on the heat sink is done after. (Section 3.2)

3.1. Soldering to the PCB, then mounting to the heat sink

If module is assembled with the PCB first and heat sink mounting is conducted later, process flow described in Figure 7 and Figure 8 is recommendable. Firstly, the module is placed on the PCB until the lead stopper contacts with the PCB (a). Then, soldering to PCB is done (b). Minimum distance between PCB and heat sink is designed to be H₁ and the distance between module and PCB is H₂, as described in Table 6.

Manual soldering and wave soldering are the general practices to assemble the module onto the PCB. At manual soldering, both bottom side and top side soldering is available. Wave soldering system consists typically of solder fluxing, preheating zone, solder wave and the cooling zone. As the board enters the conveyorized process, solder flux is sprayed or foamed onto the modules. Then it moves to the preheating zones, normally done by convection, where the flux is activated. The assembly then moves to wave soldering. The assembly is slowly cooled down after.¹⁾ More details about the soldering process and the conditions for SPM 2 packages are described in Section 6.

(a) Place the module on the PCB until the stopper touch the PCB surface.



(b) Soldering the pins to the PCB (wave or manual soldering).



Figure 7. Process flow of soldering a SPM 2 package (When PCB mounting first) I

Table 6.	Specification	of H1 an	d H2
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	H1	H2	H3
SPM2 32 L	7.20 mm	0.98 mm	8.18 mm
SPM2 34 L	8.00 mm	1.00 mm	9.00 mm

After PCB assembly is done, TIM (Thermal Interface Material) is applied on the surface of DBC or heat sink (c). Place module onto the heat sink and screws to the heat sink (d). Recommendable TIM application and screw tightening method are followed in Section 4 and 5.

(c) Apply thermal interface material on the module or heat sink surface



 (d) Place the module onto the heat sink and fasten the screws (Without spacers between PCB and heat sink.) Refer to Section 5.2 for more detail procedure



Figure 8. Process flow of mounting a SPM 2 package (When PCB mounting first) II

3.2. Module mounting to the heat sink first, then soldering to the board

When the module is mounted onto the heat sink before PCB mounting, a process flow as illustrated in Figure 9 is recommendable. Firstly, apply TIM on the surface of DBC or heat sink and place the module on the heat sink (a). Tighten the screws down to heat sink (b). Then the module with the heat sink is placed onto the PCB (c). Finally, the solder joint between pins and PCB is formed (selective soldering process, manual) (d).

(a) Apply thermal interface material on the module or heat sink surface and place module onto the heat sink



(b) Tighten up the modules with the heat sink using M4 screw.



(c) Place the PCB until the stopper touch the PCB surface.(d) Soldering the pins to the PCB



Figure 9. Process flow of a soldering for SPM 2 package (When heat sink mounting first)

3.3. System considerations

After module is assembled to the PCB and the heat sink as described above, the overall structural integrity needs to be considered in terms of mechanical stress to any of the system components. In case the PCB is large and heavy with other components assembled to it, there is some risk the PCB can bend, creating mechanical stress to the module and the PCB. In addition, when multiple modules are applied to the same PCB, height tolerance between modules can result in mechanical stresses to the board and modules. As an option, to reduce stress, spacers should be added on the heat sink, as illustrated in Figure 10, to prevent any possible movement of the PCB.

(c) Add spacers if necessary.



(d) Place the PCB until the stopper touch the PCB surface. Previous a soldering process, screwing the PCB with spacer if spacer is between heat sink and PCB.



(e) Soldering the pins with PCB.



Figure 10. Process flow of a soldering for SPM 2 package (When spacers applied between PCB and heat sink)

Figure 11 shows examples of spacer type. Option 1 shows individual spacers between heat sink and PCB. Option 2 shows a special shape of heat sink. And, option 3 is the spacer mounted between module and the PCB.



Figure 11. Examples of the spacer type

When the stopper of the pin touches the PCB the distance between PCB and heat sink is 7.2 mm for 32L and 8.0 mm for 34L. Therefore, the height of the spacer should be designed to be 7.2 (+0.1/-0.1) mm and 8.0 (+0.1/-0.1) mm.

© 2014 Fairchild Semiconductor Corporation Rev. 1.0.0 • 9/23/16 Minimum height of spacer



Figure 12. Height of spacer and air gap

4. Thermal Interface Materials (TIMs) for electronics cooling

Since the contact surfaces are not perfectly flat, multiple air gaps can form between two solid contact surfaces. Air is a poor heat conductor preventing the heat transfer and limiting the effective contact area. Thermal Interface Materials (TIMs) need to be applied between the heat sink and the DBC surface of the module to fill any air gaps and to achieve a low thermal resistance. **Appendix I** shows thermal resistance results comparing the assembly with and without TIM.

The following are the general considerations when choosing the material for the application. Besides its thermal conductivity also handling and rework performance may be important factors while selecting the proper TIM.

- High thermal conductivity
- Ease of distribution with low contact pressure
- Minimal thickness
- Degradation of characteristics over time
- Environmental
- Ease in handling during application or removal

Though thermal interface materials with improved performance are available nowadays, still the most commonly used in the industry is thermal grease. Thermal greases consists of silicone or hydrocarbon oils that contain various fillers which have good surface wetting characteristics and flow easily to fill voids even at low mounting pressure. Standard thermal compounds have a thermal conductivity between 0.7-0.9 W/m-K while the thermal conductivity of high end compounds is in the range of 2.0–4.0 W/m-K or even above. As an alternative PCM (Phase Change Material) provide improved reliability and high thermal performances as well as lower overall costs due to a simplified assembly process. It is recommended to contact your local Fairchild representative for more information regarding PCM preapplied modules.

2.3.1 Manual TIM application

Thermal grease can be applied to the heat sink or the module back side using a rubber roller or spatula or by screen printing. A rubber roller, as shown in Figure 13, is an easy and fast method for applying thermal grease. Since the thermal grease has the lowest thermal conductivity in the thermal path, a layer as thin as possible is necessary to keep the overall thermal resistance low. Recommended thickness of printing layer is uniform dispense of a minimum 150 um. The thermal grease thickness can be checked using thickness gauges, such as wet film combs or wet film wheels. Figure 8 illustrates the application of thermal grease on the product. Since manual control of printing is needed to achieve a technique for good quality printing in the application.



Thermal grease is applied on the heat sink evenly using the rubber roller. Firstly, thermal grease can be distributed in <u>parallel</u> <u>direction</u> with rolling repeatedly.



Then, thermal grease is applied in <u>vertical direction</u> with rolling repeatedly.



Thermal compound being applied to the device in vertical direction with several repetitions of rolling.

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Figure 13. Example of thermal paste application using a rubber roller

2.3.2 TIM application by manual screen printer

Stencil/screen printing can be utilized for the application of thermal paste It allows a fast, clean and easy handling of spreadable TIMs. They can be applied to the DBC area, leaving out other parts of the module package using specifically designed stencils. An optimization of the screen mask pattern and thickness is required to achieve a good quality of the print and finally an optimum contact. Figure 14 shows an example of thermal paste application process using a manual screen print.



Place the module on the mounting jig. Ensure the DBC area is clean. (Sample is APM 19)



Place the squeegee or spatula behind the TIM and tilt down it to have 45° angle around. Apply a certain pressure and draw the squeegee downwards

Maintaining the constant printing pressure and speed make possible to achieve uniform pattern of printing laver.



Lift the screen mask and do visual inspection after application

Example (APM 19 Package) of thermal paste Figure 14. application using a manual screen print

Fully automated screen printing is recommended in mass production. It a good quality of printing layer with high accuracy and repeatability.

5. Screw tightening guideline

5.1 Screw and mounting torque

SPM 2 package should be secured on the heat sink via two M4 screws. The location of the screw holes are illustrated in Figure 15. Table 7 shows the screw specification and Table s 8-9 are showing the recommended torque ranges for the SPM 2 Packages. Contact pressure and mounting torque may affect the thermal performance. The thermal resistance specified can be achieved with the minimum specified torque in the table 8-9. **Appendix II** shows thermal resistance variance under various torque levels. Electric screwdrivers can tighten the screws with the specified torque. Considering the electrical spacing specified in Section 2.4, additional flat or spring washers can be applied on packages during mounting. Figure 16 shows SEMS (Preassembled washers and screw) which is a recommended screw type.

SPM 2 -32L







Figure 15. Dimension of screw clamping zone (mm)

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Parameter	Description	
Mounting	Metric 4 screw	
Spring washer	$D = \emptyset 7.0 \text{ (mm)}$ to DIN 127 or DIN 128	
Plain washer	$D = \emptyset 9.0 \text{ (mm) to DIN 125}$	
Recommended thread engagement for screws with		
property class 4.8 to 6.8 for different materials		

Table 8. Mounting torque specification for \$	SPM 2	32L
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Parameter	Unit	Min.	Тур.	Max.
Pre-Torque	[N·m]	0.2		0.4
	[kgf·cm]	2.0		4.1
Final Targue	[N·m]	0.78	0.98	1.17
Final loique	[kgf·cm]	8.0	10.0	12.0
Generally, pre-torque is 20-30 % of the final torque				
Recommended final torque is 0.98 N·m				

Table 9. Mounting torque specification for SPM 2 34L

Parameter	Unit	Min.	Тур.	Max.
Pre-Torque	[N·m]	0.2		0.4
	[kgf·cm]	2.0		4.1
Final Torque	[N·m]	0.9	1.0	1.5
	[kgf·cm]	9.1	10.1	15.1

Generally, pre-torque is 20-30 % of the final torque Recommended final torque is 1.0 $N{\cdot}m$



Figure 16. SEMS (Pre-assembled washers and screw, spring washer ø 7.0 and plain washer ø 9.0)

5.2 Screw tightening method

Screw tightening can be done in various ways. Figure 17 describes one recommended method for fastening the module to the heat sink. Example module is SPM2 34L. Fasten two screws with final torque simultaneously to prevent tilting or rising of one side of module during fastening. The recommended final torque (M_{torque}) is in the range of 0.9-1.5 Nm (9.1- 15.1 kgf·cm), as shown in Table 8. Method 1 enables to maintain an even thermal grease layer after mounting.





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Alternatively, Figure 18 shows another recommended method to tighten the screws. Fasten the first screw with pre-torque to prevent one side tilting or rising of the module (Step 1). Then insert the second screw to the other side with same pre-torque (Step 2). The pre-screwing torque is set to 20~30 % of final torque rating. After that, apply full final torque to the first screw (Step 3). Finally, apply full torque to the second screw for proper mounting to the heat sink (Step 4). An insufficient tightening torque may cause an increased thermal resistance or loosening of the screws during operation.

Pre-torque



Figure 18. Illustration of screw clamping with heat sink (Method 2)

Note:

- Avoid applying over torque when mounting screws. Excessive fastening force may cause damages to the semiconductor devices, the package or its isolation, as well as damages to the screws or heat-sink.
- Uneven mounting can cause the SPM ceramic substrate to be damaged. A smooth surface free of burrs and protrusions or indentations is required (Table 2). No

foreign materials except thermal interface materials are allowed between DBC of the module and the heat sink.

• The mounting area should be treated as a functional layer. Do not touch the mounting area of the heat sink and the substrate of the module.

5.3 Potential failure modes

The following are possible root causes of mounting failures which should be avoided during the mounting process. Table 10 lists representative examples of mounting failure mode.

- Excessive torque is applied without pre-torque
- Misalignment of screw during tightening with heat sink
- Mechanical stress by mounting height tolerances when multiple module mounted on the same PCB
- Inappropriate type of screws are used

Table 10. Examples of	mounting failure mode (Various
types of SPM packages)	

Failure mode and	Example
cause	
1) EMC broken due to too high torque	
2) Package crack by abnormal heat sink flatness	
3) Ceramic crack by abnormal heat sink flatness	

6. Soldering Guidelines

Wave soldering or hand soldering are the general practice for through-hole type (THT) components. This section assesses characteristics of the soldering process for SPM 2 modules at the assembly to a PCB (Printed Circuit Board).

6.1 Wave soldering

Assemblies are placed on a carrier belt moving through the soldering process contacting a solder wave. The wave soldering process typically uses a thermal profile which consists of four stages: solder fluxing, preheating zone, solder wave and cooling zone. Solder flux is either sprayed or foamed onto the components. Then the parts move to the preheating zones, normally done by convention, where the flux is activated. The assembly then moves to wave soldering and finally is getting cooled down slowly.¹⁾ Key elements such as preheat ramp rate, conveyor speed, peak temperature and time forms a wave solder profile. The wave soldering profile should be optimized in the assembly site since it strongly depends on the equipment condition and the material type used in application. A typical soldering profile and its conditions are illustrated in Figure 19 and Table 11.

Preheat: Preheating is required to avoid thermal stress due to overheat. Preheat temperatures and the preheating time should be set according to the flux specification. Too high temperature and too long preheat time may break down the flux activation systems which causes shorts. On the other hand, too low preheat temperature may cause unwanted residues left on the PCB.^{1) A r} amp up rate between 1~4 °C per second is suggested in the preheat zone.

Wave soldering: Dual-wave soldering is the most common method. The 1^{st} wave which has turbulent wave crest ensures wetting of all the land pads allowing the molten solder to find its way to all joints on the PCB. The 2^{nd} wave, which has a laminar flow, drains the excess solder from the board after the 1^{st} wave thus removing the solder bridges.¹⁾ It is recommended to keep the maximum soldering temperature up to 260° C for 10 sec to establish a good quality of the solder joint and to avoid package damage by thermal shock.

Cooling: Gradually cool the processed board down. A cooling down rate between 1 - 5 $^{\circ}C/s$ is recommended in general.





Table 11. Typical dual wave soldering condition (at external terminals)

Profile	SnPb eutectic	Pb-free
Feature	assembly	assembly
Average ramp up rate	~200 °C/sec	~200 °C/sec
Preheat ramp up rate	Typical 1-2, max 4°C/sec	Typical 1-2, max 4°C/sec
Final preheat temp.	~130 °C	~130 °C
Peak wave soldering temperature	max 235 °C, max 10 sec	max 260 °C, max 10 sec
Ramp down rate	5°C/sec max	5°C/sec max

Detailed conditions of the soldering profile should be defined by users as it depends on the equipment and the materials.

6.2 Manual soldering

The recommended conditions for manual soldering are listed in Table 12. Considering the glass transition temperature (Tg) of the package mold resin and the thermal withstand capability of internal chips and assembly, the temperature of the terminal root part should be kept below 150°C. Iron tip should touch the lead terminal at its tip, away from the package mold body.

Manual soldering is not recommended for mass production as it may be difficult to control the amount of solder applied and the time and temperature of the soldering step.

 Table 12. Example of manual soldering condition

Parameter	Single side circuit board	Double/multi layers circuit board
Iron tip temperature	385 ± 10 °C	420 ± 10 °C
Soldering time	2 ~ 6 seconds	4 ~ 10 seconds

6.3 Soldering quality inspection

Monitoring the soldering quality is essential since abnormal solder joints are potential risks. IPC-A-610 standard specifies the soldering quality criteria for soft soldering. For the examination of a solder joint, visual or X-ray inspection and automatic optical inspection (AOI) are suitable evaluation methods.

Appendix I

Thermal performance under various mounting torque³⁾

Since the module surface and heat sink are not perfectly flat, contact pressure and mounting torque can affect thermal performance. AN-9079 shows a correlation between the mounting torque and the thermal resistance for a 1200 V Motion SPM 2 module. According to the results shown in Figure 20, higher thermal resistance values (Rthjc) were measured at low torque levels ranging between 1~4 (kg·f-cm) while the thermal resistance reaches lower and stable values above 5 (kg·f-cm) torque.



Figure 20. Thermal resistance under various mounting torque

Literature

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- [6] JEDEC, JESD22-B102D, "Solderability," VA, Sept. 2004.

Related Datasheets

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